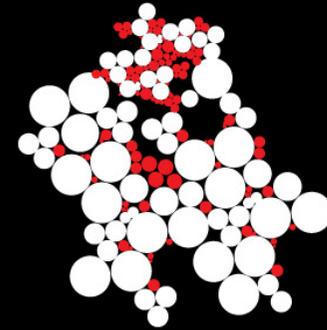


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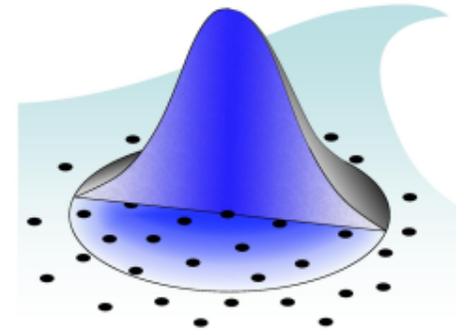


An Introduction to Smoothed Particle Hydrodynamics

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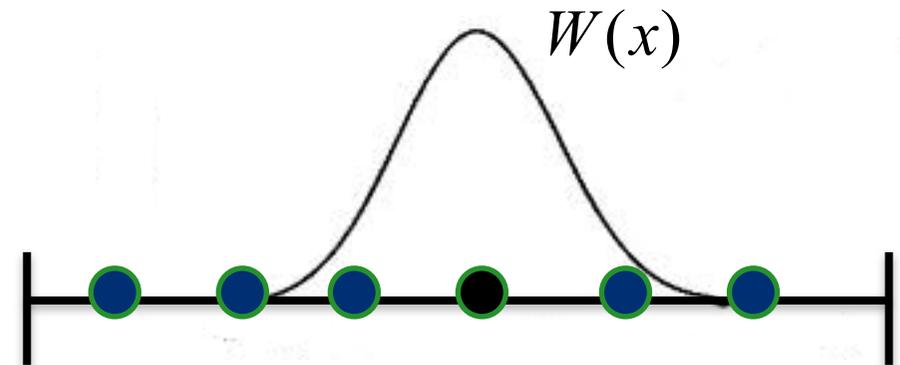
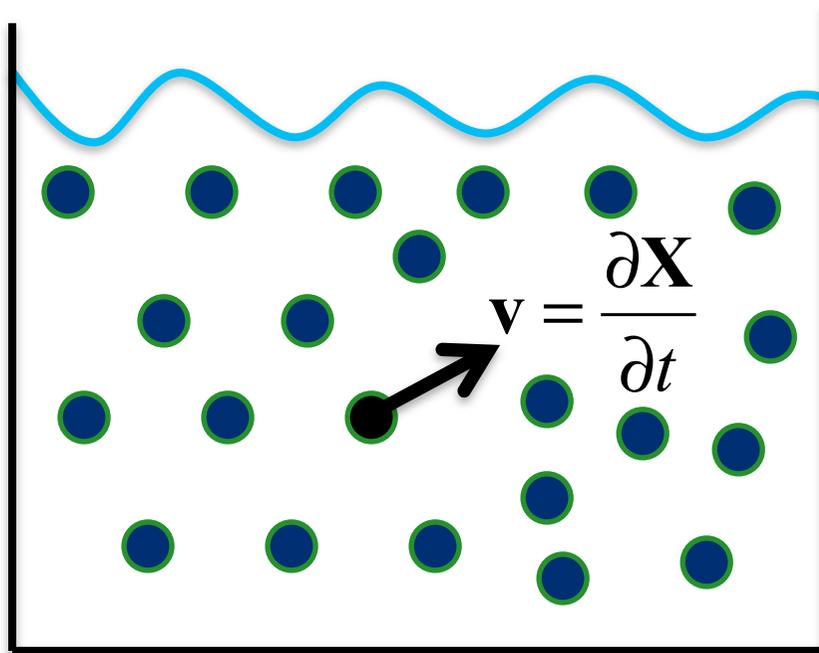
Outline

1. Introduction to SPH

- Kernel Interpolation
- First and second derivatives
- Derivation of main SPH equations

Smoothed Particle Hydrodynamics

- Smoothed Particle Hydrodynamics is a **Lagrangian** scheme
- The fluid is discretised into **particles** that move with the fluid velocity

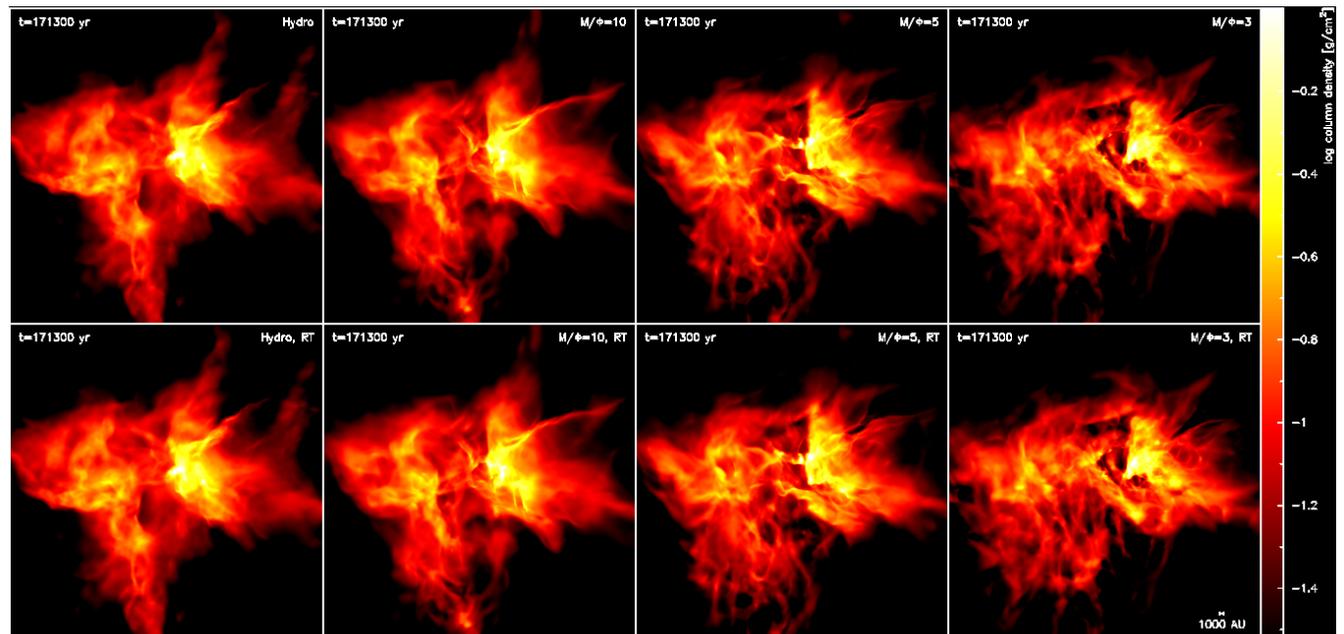


- Fluid variables are interpolated between particles using **kernel interpolation**.

Introduction

- Grew out of the astrophysics community in the late seventies
 - Gingold, R. A. & Monaghan, J. J. (1977), 'Smoothed particle hydrodynamic: theory and application to non-spherical stars', *Monthly Notices of the Royal Astronomical Society* **181**, 375–389.
 - Lucy, L. B. (1977), 'A numerical approach to testing the fission hypothesis', *The Astronomical Journal* **82**(12), 1013–1924.

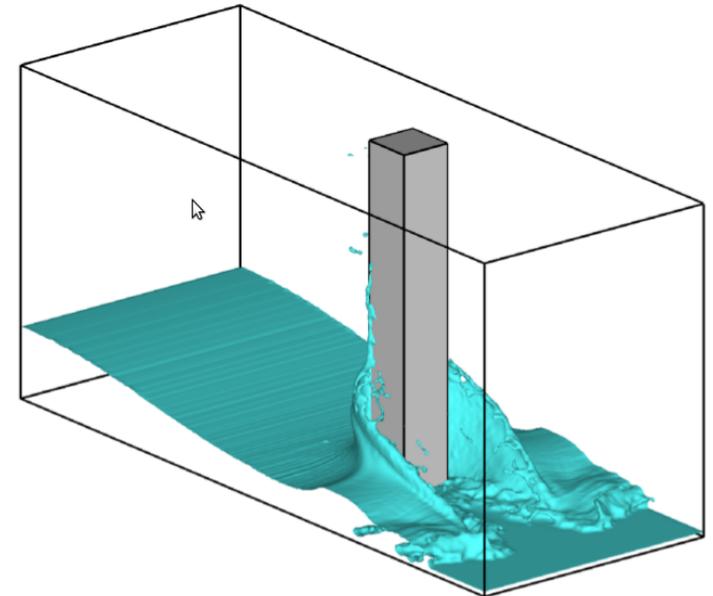
Price, D.J., Bate, M.R., 2009, Inefficient star formation: The combined effects of magnetic fields and radiative feedback, *MNRAS* 398, 33-46



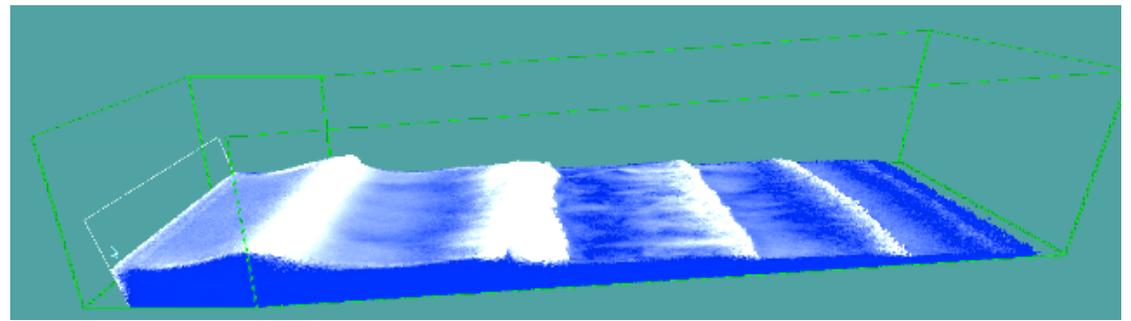
Introduction

Some advantages:

- Lack of mesh simplifies problems involving complex, moving and deforming geometries (e.g. Solid fracture), **free surfaces** and **multi-phase / interfaces**.
- Advection is obtained from the movement of the particles and the time history of fluid particles is easy to obtain (e.g. Mixing visualisation/measurement).
- Strong **conservation** properties for energy, linear and angular momentum.
- No computational effort
... if there is no mass.



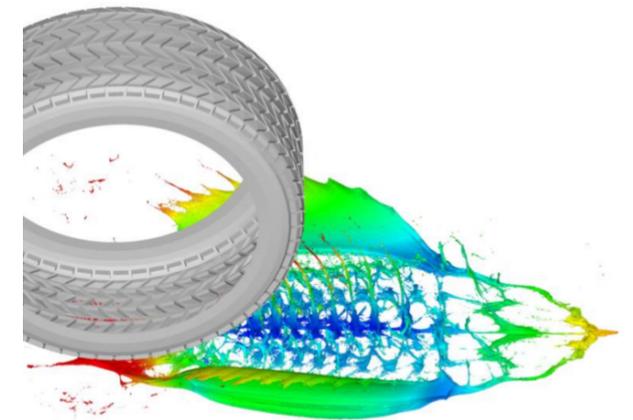
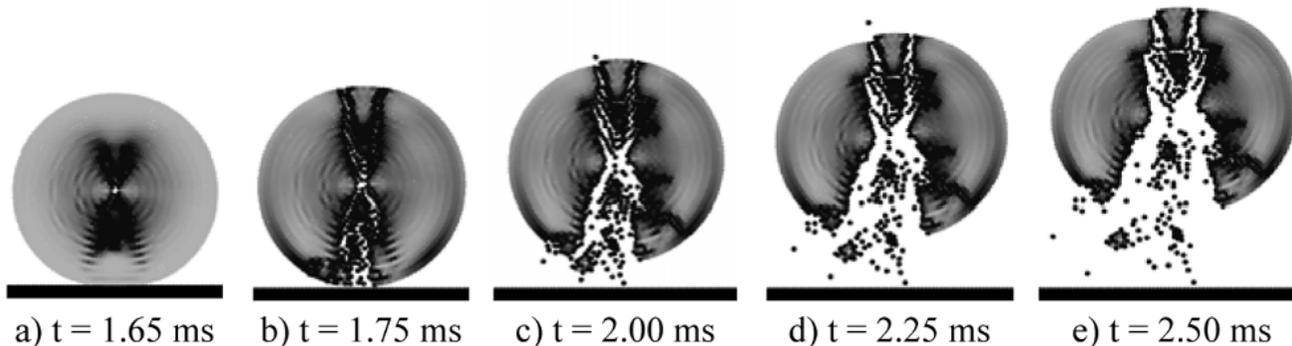
Marrone S., Colagrossi A., Le Touz´ D., Graziani G. (2009) A fast algorithm for free-surface particles detection in 2D and 3D SPH methods, *Proc. Of 4th SPHERIC Workshop*, 61-68.



Introduction

Common Application Areas:

- **Astrophysics** (e.g. Binary star systems, shocks, impact of planetesimals)
- **Marine or coastal hydrodynamics** (e.g. Breaking waves, sloshing in gas tankers, gravity currents)
- Fluid Structure Interaction
- **Industrial flows** (e.g. die casting, resin transfer moulding, sag mills)
- Deformation or fracture of **brittle or elastic solids**



Reddy, B. D., Cleary, P., Das, R. (2008) The Potential for SPH Modelling of Solid Deformation and Fracture, *IUTAM Symposium on Theoretical, Computational and Modelling Aspects of Inelastic Media*, 287-296

Oger G., Leroy C., Jacquin E., Le Touzé D., Alessandrini B (2009) Specific pre/post treatments for 3-D SPH applications through massive HPC simulations, *Proc. Of 4th SPHERIC Workshop*, 52-60.

SPH Basics – Kernel Interpolation

- Smoothed Particle Hydrodynamics is a **Lagrangian scheme**, whereby the fluid is discretised into particles that move with the fluid velocity
- Navier-Stokes equations are discretised using **kernel interpolation** between particles.

$$A_I(x) = \int A(x')W(x - x', h)dx'$$

Integral
Interpolant

$$A_S(x) = \sum_b A_b W(x - x_b, h) \frac{m_b}{\rho_b}$$

Summation
Interpolant

$$A_a = \sum_b A_b W(x_a - x_b, h) \frac{m_b}{\rho_b}$$

Calculated on
particle *a*

SPH Basics – Kernel Interpolation

- SPH Kernels are **Gaussian-like** with a compact support
- Cubic Spline kernel commonly used:

$$W(q) = \frac{\beta}{h^d} \begin{cases} 4 - 6q^2 + 3q^3 & \text{for } 0 \leq q < 1 \\ (2 - q)^3 & \text{for } 1 \leq q < 2 \\ 0 & \text{for } q > 2 \end{cases}$$

where $q = |r / h|$

$$\int W(r - r', h) dr' = 1 \quad \longrightarrow \quad \text{therefore } \beta = 1/6, 15/(14\pi) \text{ and } 1/(4\pi)$$

for one, two and three dimensions, respectively

SPH Basics – Kernel Interpolation

- SPH kernels are normally made symmetric
- This ensures **symmetric force contributions** between particles and conservation of linear and angular momentum

$$A_a = \sum_b m_b \frac{A_b}{\rho_b} W_{ab}$$

$$W_{ab} = W(x_a - x_b, 0.5(h_a + h_b))$$

or

$$W_{ab} = 0.5(W(x_a - x_b, h_a) + W(x_a - x_b, h_b))$$

Example – interpolate density

$$A_a = \sum_b m_b \frac{A_b}{\rho_b} W_{ab}$$

$$\rho_a = \sum_b m_b \frac{\rho_b}{\rho_b} W_{ab}$$

Let $A = \rho$

$$= \sum_b m_b W_{ab}$$

Example – interpolate density

$$\rho_a = \sum_b m_b W_{ab}$$

- **Physical interpretation:**

SPH particles represent a constant mass of fluid

- Density field is particle mass smoothed according to the kernel
- Particle smoothing length can vary according to density:

$$h_a = \sigma \left(\frac{m_a}{\rho_a} \right)^{1/d}$$

Ideally, iterate the calculations of h and σ each timestep, until they converge

Example – interpolate velocity (simple minded)

$$A_a = \sum_b m_b \frac{A_b}{\rho_b} W_{ab}$$

$$\mathbf{v}_a = \sum_b m_b \frac{\mathbf{v}_b}{\rho_b} W_{ab}$$

Let $A = \mathbf{v}$

Example – interpolate velocity (optimized version)

$$\mathbf{v}_a = \frac{1}{\rho_a} (\mathbf{v}\rho)_a$$

$$A_a = \sum_b m_b \frac{A_b}{\rho_b} W_{ab}$$

$$= \frac{1}{\rho_a} \sum_b m_b \frac{\mathbf{v}_b \rho_b}{\rho_b} W_{ab}$$

$$= \frac{1}{\rho_a} \sum_b m_b \mathbf{v}_b W_{ab}$$

Shepard Correction

- Use **Shepard correction** to make interpolation more accurate near boundaries/free surface:

$$A_s(x) = \frac{1}{\sum_b \frac{m_b}{\rho_b} W_{ab}} \sum_b m_b \frac{A_b}{\rho_b} W_{ab}$$

- Correction denominator is ~ 1 for kernel summations with full support, but < 1 near a free surface or some boundaries

Interpolation of Derivatives

- First approach:

$$\nabla A_a = \sum_b \frac{m_b}{\rho_b} A_b \nabla_a W_{ab}$$

- But, does not vanish when $A(x)$ is constant! Instead use:

$$\nabla A = \frac{1}{\Phi} (\nabla(\Phi A) - A \nabla \Phi)$$

$$\nabla A_a = \frac{1}{\Phi_a} \sum_b m_b \frac{\Phi_b}{\rho_b} (A_b - A_a) \nabla W_{ab}$$

$$\nabla \cdot \mathbf{a}_a = \frac{1}{\Phi_a} \sum_b m_b \frac{\Phi_b}{\rho_b} (\mathbf{a}_b - \mathbf{a}_a) \cdot \nabla W_{ab}$$

Φ is any
continuous
field

Interpolation of Derivatives

- For a radially symmetric kernel:

$$\begin{aligned}\nabla_a W_{ab} &= \frac{r_{ab}}{|r_{ab}|} \frac{\partial W}{\partial r} \\ &= \frac{r_{ab}}{|r_{ab}|} \frac{1}{h} \frac{\partial W}{\partial q}\end{aligned}$$

Example – Continuity Equation

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{v}$$

- Use SPH derivatives to evaluate divergence of velocity

$$\nabla \cdot \mathbf{a}_a = \frac{1}{\Phi_a} \sum_b m_b \frac{\Phi_b}{\rho_b} (\mathbf{a}_b - \mathbf{a}_a) \cdot \nabla W_{ab}$$

Let $\mathbf{a} = \mathbf{v}$
Let $\Phi = \rho$

$$\begin{aligned} \frac{d\rho_a}{dt} &= \rho_a \left[\frac{1}{\rho_a} \sum_b m_b \frac{\rho_b}{\rho_b} (\mathbf{v}_a - \mathbf{v}_b) \cdot \nabla W_{ab} \right] \\ &= \sum_b m_b \mathbf{v}_{ab} \cdot \nabla W_{ab} \end{aligned}$$

Example – Internal Energy

- From first law of thermodynamics:

Heat added = 0

$$Tds = dU - PdV$$

$$dV = (m/\rho^2)d\rho$$

u is internal energy per unit mass

$$0 = du - \frac{P}{\rho^2} d\rho$$

$$\frac{du}{dt} = \frac{P}{\rho^2} \frac{d\rho}{dt}$$

$$\frac{du_a}{dt} = \frac{P_a}{\rho_a^2} \sum_b m_b \mathbf{v}_{ab} \cdot \nabla W_{ab}$$

Example – The Pressure Gradient

- Momentum equation from Euler equations:

$$\frac{D\mathbf{v}}{Dt} = -\frac{1}{\rho} \nabla P$$

$$\nabla A = \frac{1}{\Phi} (\nabla(\Phi A) - A \nabla \Phi)$$

Let $A = P$
Let $\Phi = 1/\rho$

$$\begin{aligned} \frac{1}{\rho} \nabla P &= \frac{1}{\rho} \rho (\nabla(P/\rho) - P \nabla(1/\rho)) \\ &= \nabla(P/\rho) - \frac{P}{\rho^2} \nabla \rho \end{aligned}$$

Example – The Pressure Gradient

- SPH Momentum equation becomes...

$$\frac{D\mathbf{v}}{Dt} = -\frac{1}{\rho} \nabla P = -\nabla(P/\rho) + \frac{P}{\rho^2} \nabla \rho$$

Convert to SPH
derivatives

$$\frac{d\mathbf{v}_a}{dt} = -\sum_b \frac{m_b}{\rho_b} \left(\frac{P_b}{\rho_b} \right) \nabla_a W_{ab} + \frac{P_a}{\rho_a^2} \sum_b \frac{m_b}{\rho_b} (\rho_b) \nabla_a W_{ab}$$

$$= -\sum_b m_b \left(\frac{P_a}{\rho_a^2} + \frac{P_b}{\rho_b^2} \right) \nabla_a W_{ab}$$

Artificial Viscosity

- Artificial viscosity originally developed to stabilise shocks and prevent the build-up of acoustic energy due to integration errors.

$$\frac{d\mathbf{v}_a}{dt} = -\sum_b m_b \left(\frac{P_a}{\rho_a^2} + \frac{P_b}{\rho_b^2} + \Pi_{ab} \right) \nabla_a W_{ab}$$

- Modern SPH viscosity terms approximate the viscous term in the Navier-Stokes equations

Artificial Viscosity – some examples

$$\Pi_{ab} = -\frac{\alpha \bar{h}_{ab} \bar{c}_{ab}}{\bar{\rho}_{ab}} \left(\frac{\mathbf{v}_{ab} \cdot \mathbf{r}_{ab}}{r_{ab}^2 + \epsilon \bar{h}_{ab}^2} \right) \quad \text{Monaghan and Gingold (1983)}$$

$$\Pi_{ab} = -\frac{16\mu_a\mu_b}{\rho_a\rho_b(\mu_a + \mu_b)} \left(\frac{\mathbf{v}_{ab} \cdot \mathbf{r}_{ab}}{r_{ab}^2 + \epsilon \bar{h}_{ab}^2} \right) \quad \text{Cleary (1998)}$$

- Conserve linear and angular momentum.
- But derivation is rather ad-hoc....

Second Derivatives in SPH

- Better approach:
construct a second derivative in SPH to approximate

$$\mu \nabla^2 \mathbf{v}$$

- Could try:

$$\left(\frac{d^2 v}{dx^2} \right) = \sum_b m_b v_b \frac{d^2 W_{ab}}{dx_a^2}$$

- But:
 - Sensitive to particle disorder
 - Sign of this expression can change with particle separation due to second derivative of the kernel.

Second Derivatives in SPH

- More stable and accurate -> start with an integral approximation (Cleary and Monaghan 1999, heat conduction)

$$\begin{aligned}\nabla \cdot \kappa \nabla T + O(h^2) &= \int (\kappa(r) + \kappa(r')) (T(r) - T(r')) \frac{1}{|r - r'|} \nabla W(|r - r'|) dr' \\ &= \sum_b \frac{m_b}{\rho_b} (\kappa_a + \kappa_b) (T_a - T_b) \frac{1}{r_{ab}} \frac{\partial W_{ab}}{\partial r_a}\end{aligned}$$

- (Morris 1997) applied this to the viscosity term

$$(\nabla \cdot \mu \nabla) \mathbf{v} = \sum_b \frac{m_b}{\rho_b} (\mu_a + \mu_b) (\mathbf{v}_a - \mathbf{v}_b) \frac{1}{r_{ab}} \frac{\partial W_{ab}}{\partial r_a}$$

Summary

- Navier Stokes Equations for a Newtonian fluid:

$$\rho \frac{D\mathbf{v}}{Dt} = -\nabla P + \mu \nabla^2 \mathbf{v} \qquad \frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{v}$$

- Calculate SPH derivatives using kernel interpolation:

$$\frac{d\mathbf{v}_a}{dt} = -\sum_b m_b \left(\frac{P_a}{\rho_a^2} + \frac{P_b}{\rho_b^2} + \Pi_{ab} \right) \nabla_a W_{ab} \qquad \frac{d\rho_a}{dt} = \sum_b m_b \mathbf{v}_{ab} \cdot \nabla W_{ab}$$

$$\rho_a = \sum_b m_b W_{ab}$$

- Use integral approximation for the second derivative to find the viscous term:

$$\frac{1}{\rho} \mu \nabla^2 \mathbf{v} = \sum_b \frac{m_b}{\rho_a \rho_b} (\mu_a + \mu_b) (\mathbf{v}_a - \mathbf{v}_b) \frac{1}{r_{ab}} \frac{\partial W_{ab}}{\partial r_a}$$

Example SPH algorithm

- Let's use velocity Verlet integration.....
- For each timestep:

$$r^{1/2} = r^0 + \frac{\Delta t}{2} v^0,$$

$$v^1 = v^0 + \Delta t \frac{dv}{dt}(r^{1/2}),$$

$$r^1 = r^{1/2} + \frac{\Delta t}{2} v^1$$

Example SPH algorithm

- Need to update density and h field each time-step.
Here we use the summation form of the density equation.
- For each timestep:

$$r^{1/2} = r^0 + \frac{\Delta t}{2} v^0,$$

$$h^{1/2} = F_1(\rho^0) = \sigma(m / \rho)^{1/d}$$

$$\rho^{1/2} = F_2(r^{1/2}, h^{1/2}) = \sum_b m_b W_{ab}$$

$$v^1 = v^0 + \Delta t \frac{dv}{dt}(r^{1/2}, \rho^{1/2}, h^{1/2}),$$

$$r^1 = r^{1/2} + \frac{\Delta t}{2} v^1$$

Example SPH algorithm

- Also need an (EOS) Equation Of State....
- For each timestep:

$$r^{1/2} = r^0 + \frac{\Delta t}{2} v^0,$$

$$h^{1/2} = F_1(\rho^0) = \sigma(m / \rho)^{1/d},$$

$$\rho^{1/2} = F_2(r^{1/2}, h^{1/2}) = \sum_b m_b W_{ab},$$

$$P^{1/2} = F_3(\rho^{1/2}),$$

$$v^1 = v^0 + \Delta t \frac{dv}{dt}(r^{1/2}, P^{1/2}, \rho^{1/2}, h^{1/2}),$$

$$r^1 = r^{1/2} + \frac{\Delta t}{2} v^1$$

Example SPH algorithm

- Finally add viscosity....
- For each timestep:

$$r^{1/2} = r^0 + \frac{\Delta t}{2} v^0,$$

$$v^{1/2} = v^0 + \frac{\Delta t}{2} \frac{dv}{dt}(r^{-1/2}, P^{-1/2}, \rho^{-1/2}, h^{-1/2}, v^{-1/2}),$$

$$h^{1/2} = F_1(\rho^0) = \sigma(m / \rho)^{1/d},$$

$$\rho^{1/2} = F_2(r^{1/2}, h^{1/2}) = \sum_b m_b W_{ab},$$

$$P^{1/2} = F_3(\rho^{1/2}),$$

$$v^1 = v^0 + \Delta t \frac{dv}{dt}(r^{1/2}, P^{1/2}, \rho^{1/2}, h^{1/2}, v^{1/2}),$$

$$r^1 = r^{1/2} + \frac{\Delta t}{2} v^1$$

Time step conditions

- Time step calculated on a Courant–Friedrichs–Lewy (CFL) condition:

$$\Delta t \ll \frac{h_a}{v_{sig}}$$

$$v_{sig} = \frac{1}{2}(c_a + c_b - 2v_{ab} \cdot \hat{\mathbf{r}}_{ab})$$

- v_{sig} is a signal velocity equal to the speed of information exchange between particles

Time step conditions

- Viscous timescale

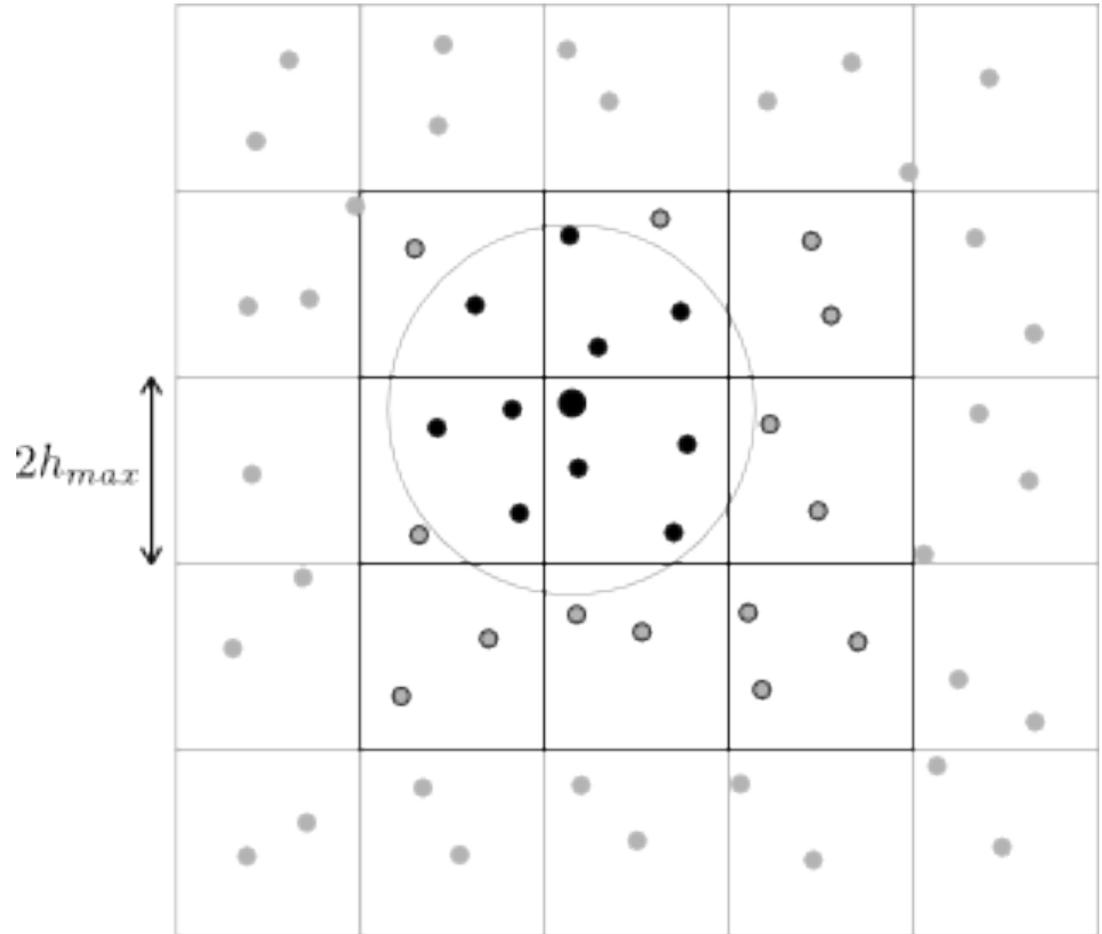
$$\Delta t \ll \frac{h_a^2}{\nu}$$

- Acceleration timescale

$$\Delta t \ll \sqrt{\frac{h_a}{dv_a / dt}}$$

Finding Neighbours – Linked Cells (like for MD)

1. Domain divided into “bins” of side length $2h_{\max}$
2. Particles placed in bins
3. Each particle’s neighbours can be found in its own bin and neighbouring bins
4. Search these bins, keeping particles within $2h$.



The End

- Exercise SPH: 1D Sod Shock using SPH....